ATMOSPHERIC NOISE MEASUREMENTS

C.N.Pq.

Data Summary Nº 1 — Station ARN-2 — Nº 10

by L. G. MEIRA Fº F. DE MENDONÇA

REPORT Nº LAFE-13 May, 1964

The measurements reported herein were performed in cooperation with the Radio Noise Section, Troposphere and Space Telecommunications Division of N B S — Boulder Laboratories.

Comissão Nacional de Atividades Espaciais São José dos Campos São Paulo — Brasil

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A B S T R A C T

Under the designation of Project "OBRA", one of the 16 atmospheric noise receiving stations of the world-wide net work supervised by the NBS, has been in operation at this Laboratory since August 1963.

This report is intended to account for the work done under this project up to December 1963, including the transference of the whole station from its early site, repairing the equipment and collecting data.

Also, the initial sections of the report outline the general problem of radio noise measurements and describe the techniques and equipment used.

Data are presented as they were obtained, without any attempt to reach conclusions. This will possibly be done later.

I. INTRODUCTION

Under a very general viewpoint, noise could be regarded as any fluctuation of a DC value in space or time, or better, human independent variations. In communication systems by radio, controlled variations of some magnitudes (voltages, fields, etc.) are used to transmit information. It is obvious that aleatory variations, overlapping those controlled, will tend to mask them; in other words, noise destroys information.

In systems operating below about 30 Mc/s one of the chief factors determining the lower limit for the power required, besides absorption, is the noise introduced at the propagation medium itself, atmospheric noise in this case. It should be noted that if such a system were considered as consisting of three parts: transmitter, medium and receiver, the second element is the only one upon which man cannot exert any influence. Hence, transmitter and receiver must be designed as to minimize unwanted characteristics introduced by the propagation medium. It follows from the above considerations that we need a detailed knowledge of atmospheric noise among the first parameters in designing a communication system at low frequencies.

An important aspect of the problem is the fact that the noise influence upon communication systems is largely dependant upon the process used. Watt et al. (1958) studied the behavior of several systems operating under thermal and atmospheric noise interference. Three processes were considered:

CW (Morse Code)

FSK (Frequency Shift Keying)

Human Voice (AM)

Among the results, we selected the best and worst conditions found, respectively:

CW, for 10% errors admitted, and 12 words per minute speed it is enough to have a signal 11.5 db below noise (rms values, for a 1 Kc/s bandwidth).

FM multiplex, 36 voice channels, for 10% errors it is necessary a signal 49 db above noise.

In both cases, transmission was under atmospheric noise, the former with steady carrier and the second subjected to tropospheric fading.

II. ATMOSPHERIC RADIO NOISE MEASUREMENTS

One could, at a first glance, conclude from what was said above that the most readly usable noise data would be those giving the percentage of errors expected from given systems and conditions or, inversely, the signal level necessary to keep errors below a certain percentage.

In fact, measurements have been made this way. However, it would be impracticable to carry them out in a large scale (continuous measurements for several places and several systems). Besides, the large number of factors envolved would make comparison between different observer's data impossible.

Hence, noise parameters were looked for which had a more precise mathematical meaning and would therefore make comparisons easier. Thus a re-

lation would be established between the parameters and the resulting interference for any desired system, as in the paper by Watt mentioned above.

Many approaches were attempted, holding different compromises between the precise meaning of parameters, their relationship to the interference, and the easiness of their measurement.

It is commonly accepted that interference on all common kinds of communication systems is determined by the noise amplitude characteristic; its determination has therefore deserved special interest from the investigators.

Many used methods make an integration of the noise envelope, with averaging periods of several minutes. Some of them are:

- average value of the noise envelope (1st moment).
- rms values of the noise envelope (2nd moment).
- ratio between 1st and 2nd moments; has as advantage an easier calibration.

Examples of other kinds of measurements are:

- "crossing rate" measurements; the number of times a given (variable) level is crossed in the upward direction is counted. Good results attained at VLF.
- "quasi-peak" detection; a capacitor is charged with a small time constant and discharges through a large one. The values of the time constants are chosen to follow some characteristics of the human ear. However, the results are of difficult interpretation.
- as a complement to "crossing rate" measurements it is useful to measure the time interval between peaks above a reference, or any other time function that will yield information about the pulse spacing distribution.

A good characterization of noise can be obtained through the amplitude probability distribution (APD) function of the voltage envelope.

This function can be determined directly by measuring the percentage of time a given level is exceeded and varying this level. Crichlow et al. (1960) presented an indirect method in which the APD function is determined through three of its statistical moments. Section 4 of this report presents a brief description of the method.

III. ATMOSPHERIC NOISE VARIATIONS

Atmospheric radio noise variations are random in nature and must be treated statistically. However, some regularities are observed for long term variations, and among them we have:

- diurnal variations; in a general way noise levels are higher at night time, as the best propagation conditions are found at these hours. Noise levels are usually higher in the afternoon than at morning, as thunderstorms are more frequent after midday.
- yearly variations; thunderstorm centers shift from equator to tropics from summer to winter; although absorption is greater on summer, there is an increase in noise levels during this season.
- by intrinsic conditions to the physical processes of atmospheric noise generation by thunderstorms and wave propagation, noise levels decrease with frequency. At frequencies of about 10 Mc/s, however, cosmic or man-

-made noise can become the predominant one, depending on local meteorological conditions.

- a factor affecting largely the received noise level, as well as its characteristics, is the receiver bandwidth. When it is reduced, noise level is lowered and its amplitude probability distribution is altered, tending to that of thermal noise by flattening and overlapping of the peaks.

IV. DETERMINATION OF ATMOSPHERIC RADIO NOISE AMPLITUDE PROBABILITY DISTRIBUTION BY MEANS OF THREE PARAMETERS

Noise amplitude distribution function is usually represented on a graph where the ordinade corresponds to the signal level (relative to rms value) and the abcisse to the percentage of time during which the corresponding ordinade is exceeded.

Rayleigh paper is used; its scales are built so that thermal noise, obeying a Rayleigh distribution, will plot as a straight line of slope -1/2.

When atmospheric noise is plotted this way, a curve similar to that of fig. 1 is obtained. Three regions can be distinguished in it:

- 1. low amplitude, high probability region; distribution is practically Rayleigh, as it is composed of many overlapping pulses like thermal noise.
 - 2. approximately an arc of circunference.
- 3. high amplitude, low probability signals (separate pulses). Distribution plots almost linearly.

A curve of this kind can be perfectly characterized through 4 parameters. As for atmospheric noise an experimental relationship can be derived between two of them (Crichlow, et al. 1959), one need to measure only 3 of them to characterize perfectly the curve.

The parameters adopted by the National Bureau of Standards to be measured by the ARN-2 stations are the three which follow:

V_{rms} = root mean square value of noise envelope.

 L_{d} = ratio between the rms value and the logarithmic average of noise voltage.

 V_d = ratio between the rms value and the average of noise voltage.

Let e be equal to $1/\sqrt{2}$ times the instantaneous envelope voltage and p(e) the probability of e being exceeded. Then

$$V_{\text{rms}} = \sqrt{\int_{0}^{\prime} e^{2} d\rho}$$

$$V_{\text{ave}} = \int_{0}^{\prime} e \, d\rho$$

$$V_{log} = antilog \int_{o}^{t} log e d\rho$$
 $V_{d} = 20 log V_{rms} / V_{ave}$
 $L_{d} = 20 log V_{rms} / V_{log}$

as defined by Crichlow et al. (1959).

Together, these three parameters give us the rms value of noise and the amplitude probability distribution APD of the difference between the instantaneous and the rms value.

APD curves for values of L_d and V_d commonly found in atmospheric noise were presented in a NBS Monograph (1960). The validity of such curves has been checked by comparison with others obtained directly.

V. THE ATMOSPHERIC RADIO NOISE STATION ARN-2

The National Bureau of Standards developed the equipment for continuous measurement of radio noise during IGY. It was called ARN-2 station and 16 of them were installed in a world-wide net.

The station operates on 8 channels of fixed frequency, two of which are recorded each time during 15 minutes. At the end of this period the two next channels are connected so that one sample for each frequency is obtained at the end of every hour. Fig. 2 shows the block diagram for a single channel. Automatic switching units were omitted for the sake of clarity.

The sampling interval is 15 minutes and the value thus obtained is taken as representative of the noise level through the whole hour. The log and linear deviation recorders operate on a single frequency. They are connected to four of the channels during one week and to the remaining four during the next one, so that all the eight channels are scanned.

In synthesis, the system is a receiver of unusual stability and selectivity, bandwidth of about 200 cps. The parabolic amplifier after the IF section allows the detected signal to be proportional to the square of the envelope voltage, the rms value being hence obtained by integration. The signal at the integrator output is kept at a constant level by means of a feedback loop in which the deviations of the integrated signal from reference will cause the attenuator at the IF input to move in such a way that the deviations are compensated. A chart strip recorder working as a servo of the attenuator registers the rms value of the noise envelope.

Part of the IF signal is picked up at the second IF amplifier output and after amplified and detected, is fed into linear and logarithmic amplifiers preceded by integrators. By means of suitable calibration with respect to the integrator reference level, the recorders at the output of the above amplifi-

ers record directly L_d and V_d in db below V_{rms} .

Special programming units are included which provide more reliabili-

ty on the results. For the power recorders, a programmer of the attenuator, after a frequency change in which the attenuator is reset to zero, allows it to move upwards, thus approaching the noise level from below. After three minutes, time enough for this value to be reached, the programmer moves the attenuator an aditional 6 or 8 db and doesn't permit any further movement in this direction. At this time the integrated output is below reference and the attenuator will move downwards, approaching noise level from above. This kind of operation avoids partially false results decurrent from sudden interferences, as noise is considered to be the lowest signal existing.

Each recorded frequency is identified by means of two auxiliary pens at the edge of the chart.

For the log and linear deviation recorders, a timer prevents them to operate unless 4 minutes have elapsed since the last attenuator step. As this interval is greater than the time necessary for the integrator to move the attenuator one step (2 db) if the signal is 1 db from reference, it becomes practically assured that the recorded deviation is in fact with respect to the rms value within a precision better than 1 db.

An alignement oscilator together with a small transmitting antenna and a temperature-limited diode operating as noise generator allow the rms (power) measurements to be referenced to an absolute level.

Summaryzing what was said above, the results of ARN-2 measurements are presented using the symbols:

 F_a = effective noise figure: external noise avaliable from an equivalent short, lossless vertical, antenna in db above kTB; this can be converted to

 E_n = equivalent vertically polarized ground wave rms noise field strength in db above 1 μ V/m for a 1 Kc/s bandwidth.

$$E_n = F_a + 20 \log_{10} f(Mc/s) - 65.5$$

T taken as 288 $^{\rm O}$ K.

 L_{d} = db value of the ratio between the rms value and the logarithmic average of the noise envelope.

 $V_{\rm d}$ = db value of the ratio between the rms value and the average of the noise envelope.

Some of the stations have also equipment for directional measurements, consisting of a National NC-183-D receiver and a horizontal Yagi in a rotary assembly.

VI. THE ARN-2 STATION Nº 10

It was seen at the preceding sections how the need for atmospheric radio noise measurements appeared, some of the adopted techniques and how a world network was stablished in 1957 supervised by the NBS.

São José dos Campos, Brazil, was chosen for installation of one of these

stations: the ARN-2 No 10, its operation being carried out by the ITA.

However, several problems related to personnel, maintenance difficulties, roof insulation leakages, and others, prevented the station from operating within the schedule; data acquisition suffered many interruptions.

Data were last recorded intermittently only until April 1962, for the

initial phase on operations.

An agreement was made by the beginning of 1963 between ITA's Electronic Enginnering Division and CNAE, the second being in charge of the operation from 1963 on. It was decided that better assistence could be given to the equipment if it were re-installed within CNAE's laboratories.

This was done starting March 1963. It follows a brief outline of the tasks

performed.

Building - a larger one was built as to make equipment maintenance easier. Special attention was given to the roof insulation to avoid the frequent leakage occurring at the older installations. See figures 9, and 10.

Antenna - the antenna system was completely dismounted and its parts submitted to cleaning and preservation processes. The ground plane posts were changed from wood to steel. At the ground plane center a copper screen was used instead of metal sheet.

Racks - all the units were removed from the racks and individually checked; the racks themselves and the front panels were re-painted. Many of the defective units (which were held over in São José dos Campos by previous operators) were used as a supply of components. The station was put into operation and developed many defects which were removed. Finally we started continuous operation on July 1963 and it has been working properly since then. As a result, the set ARN-2 has been re-integrate on the world wide system, and the data so far obtained has been of good quality. Figure 11 shows noise receiving station.

VII. RADIO NOISE DATA FROM ARN-2 STATION Nº 10, FOR THE PERIOD AUG. 63 - DEC. 63

Place: São José dos Campos - Brazil - 23.3°S - 45.8°W.

Local time: (GMT - 3 h).

Receiver: ARN-2 (NBS) with a vertical, omnidirectional antenna, with a horizontal plane of 30 meters radius.

Data is found in tables 1 to 5. The symbols used mean:

Fam = median value of daily Fa during a month for a given hour.

 $D_{\rm u}$ and $D_{\rm l}$ = upper and lower deciles of the monthly distribution for a given hour.

L_{dm} = median value of daily L_d during the month.

 V_{dm} = the same for V_{d} .

An asterisk above any median value indicates it was evaluate from less than 15 observations for F_{am} or less than 7 for L_{dm} or V_{dm} .

Although special care is taken to avoid interference in the measurements, it is possible that some times the received signal is contamined with other than atmospheric noise. In this case the value of L_d will decrease and this fact is used to mark probably contaminated data. In a study from several uncontaminated noise samples (NBS Technical Notes series 18) it was evaluated the most probable and the minimum value of L_d corresponding to each V_d that will result on an APD curve of the form expected inatmospheric noise. It is also suggested that whenever the value of L_d found is below the minimum for that V_d , the most probable value of L_d should be used instead of the one actually measured. This suggestion was followed throughout the data presented in this report. A small circle above the L_d value indicates a quantity which is not the actually measured value.

Figs. 3 to 7 present the power data in graphical form.

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 F_{am} = median value of effective antenno noise in db above ktb

Du = ratio of upper decile to median in db

De = ratio of median to lower decile in db

 V_{dm}^{\pm} median deviation of average voltage in db below mean power L_{dm}^{\pm} median deviation of average logarithm in db below mean power

TABLE 1

MONTH-HOUR	VALUES.	OF	RADKO	NOISE

Station	S.José,	Brasil

Lat. 23.39S Long. 45.89W

Month Sept. 1963

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_	116	+	9		110	14	16			88"					88	6	13			43*	<u>L</u>				60	12	23	<u> </u>		78	12	7			32		6		_
18	118	15	14		112	14	18			91	19	14			87	9	16			60	II	8			60	11	18			54	12	μ			32	20	જ		_
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	123				116	16	10			99		,				16	6			67	12	9			63		<u> </u>	<u> </u>		55)	+			37	16	9		_
_	126	+-	_		118	8	4			17	1	32			95					69	8	17			59	13	10			52	10	14			34 *				_
22	H	Ή	$\overline{}$	T 1	118	+	10			105		13			90	9	8			70					65	7	18			55	10	14			35	18	9	\sqcup	┨.
23	126	10	2		122	9	10			107	10	23			92	8	8			70	8	16	<u> </u>		65	7	16	<u></u>	<u> </u>	50	10	7			32	16	8		_J;

Form = median value of effective antenna noise in db above ktb

D_U = ratio of upper decile to median in db

 $D_{\mathcal{Z}}$ = ratio of median to lower decile in db

V_{dm}= median deviation of average voltage in db below mean power L_{den} = median deviation of average logarithm in db below mean power TABLE 2

ı	MONTH-HOUR	VALUES OF	RADIO NOISE	Station São	Jose, Brasil	Lat.23.395 Long.4	5.89W Month	October 19 63
E				Frequency	(Mc)		•	
-	.051	.113	. 246	. 545	2.5	5.0	10.0	20.0

LST																	Fr	equ	ency	(Mc)																		
		•	051				. 113	3				246	-				<u>545</u>				2	2. 5					<u>5. 0</u>				10	. 0				20	0.0		
Į Ž	Fem	D	D	Vaim Laim	Fem	Du	De	V∉m	Ldm	Fam	Du	De	Vdm	-dm	F	D	Dz	Velm	L _{den}	Fam	Du	D	∀dm	Ldm	Form	Đų	D	Vdm	Ldm	Fem	Du	De	Vdm L	Fa	m C	Du	De	Vdm	-dm
00	136	Q	5		126	9	9			l(ο	9	11			97	5	7			65	12	14			72	10	7			16	13	ħ		29	<u>)</u> (જ	3		_
01	137	7	9		127	8	11			109	8	5			94	(0	7			65	15	14			66	11	12			43	7	2		Z	g) (6	7		
02	136	9	10		127	8	11			108	H	6			96	8	10			6 4	13	11			66	lσ	14			45	12	14		20	0 1	12	7		
03	138	7	12		126	10	11			60	Ö	8			98	6	12			67	10	14			68	10	lı			45	16	15		2	1 .	8	6		\Box
04	138	7	12		126	10	13			109	9	13			98	4	í5			65	10	13			68	9	13			43	12	14		2	8 1	4	7		
05	ાઉદ	6	13		118	10	19			92	17	19			25	10	16			65	10	13			70	9	17			41	14	12		2	7 '	8	5		
06	130	9	16		111	14	22			86	7	11			१३	9	10			55	10	19			66	8	18			4,	14	14		2	1 .	8	5		
		8,			114	11	16			91		16			છે).	9				47	9	15			58	$\overline{}$	11			47	7	15		2	7 1	6	6		\Box
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_	122				110	-		1		88.					28	16	10			29					42					31*			- 4	2	2				
_	124	T .	15		110	1	15	1		89	26	14			86		13			27					45					34	14	15		2	6				
11	1	12	1	1.	110	 	12			91					88		9				18	8			37	17	8		·	35	10	15	5.	2	71	_			
12	#	13	_		юх	1	+			93		1			88	-	8		_		26				42	12	9			39)	જ	16		20	3				
	#	_	+		113	+-	10	1		95					89		12				25	-			41	20	8			34		ક		33	31				
	130	14	+		און	 	9	1			20				89		17			*-	го					14	9			37	11	7		3	$\overline{}$		ì		
15		 	1		#	23	+ -			_	26	_			93		-			H	19				52	17	9			39	18	7		3	7*				
16		13	1		11	24	_			103					90					61	14	19		,	62	13	14			42	17	7		3	7 1	10	8		
-	138		+		124	+	15			-	23				ସଧ		_			57	-	-		_	69	9	10			43	18	5		1	o				
	136	_	10		120	+	9	1		103	_				93	-			1	*	19				73	6	7				16	7		4		16	12		
	35	+	+		IZZ	$\overline{}$	_	\vdash		107					98	_	10	\vdash	1	71	+	13			73	9	7			50	(I	9		L	_	19	16		
20	-	14	1		126	+	9	1	T	109		8			98	_	12			71	14			Н	73	-	5			50	9	7		_	3				
-	136	_			126		li I	\		109	_	_			98		11			Ti	8	10			12	8	<u>)</u> ।			45	16	7		3		9	6		
22	#	_	17	1-1-	128	' 	14	1		113	_	9			98	8	9		1	69	+	14			69	_	5				१३	9		3	_	5	6		
23	1	1	1.		126	1	1	1	†	in	7	5	$ \cdot $		99	-	9		t	65	+	15			10	10	8		\Box	43	17	7		3		-	9],

 F_{dim} = median value of effective antenna noise in db above ktb

 D_{ij} = ratio of upper decile to median in db D_{ij} = ratio of median to lower decile in db

V_{dm}= medion deviation of everage voltage in db below mean power

Line * medien deviation of average logarithm in db below mean power

TABLE 3

N	101	1TI	-	HOUR	V	٩L١	UES	S 0	F	RA)M) (NOI	SE		S	itati	on S	ão .	José	, E	3ras	il	L	at. 2	3. 3	<u> </u>	Long	g. <u>4</u> 5	5.89	•w	M	onth	N	ove	<u>mb</u> e	r 15	63	3
ST																	Fre	que	ncy	(Mc)																		\neg
13			051				. 11	13				. 24	 6				545				2	2. 5		-		5	. 0				10	0.0				20	0.0		\neg
롿	Fam			Vdm Ldm	Fam	Du	De	Vdm L	dm	Fam	Du	D,	V _{dm} L	-dm	Fam	Du	D,	V_{dm}	Ldm	Fam	Du	D ₂	Vdm	Ldm	Fam	Du	D	Vdm	L-dm	Fom	Du	De	Vdm	L-dm	Fam	٥u	DL	Vdm L	-dm
00	139	7	6		119	Į1	11			99	13	Į)			92	SI	9			74	g	7			63	16.	8			37	14	13			28	4),		\Box
01	140	5	9		119	11	17			100	9	14			94	13	18			73	13	ר. [55	SO	1			38	0	13			28	П	5		
02	138	6	12		117	lı	24			101	9	13			93	9	17			74	Ø	Ħ			55	17	ΙO			38	10	14			26	g	4		
	138		10		119	10	18			98	10	13			93	0	20			72	14	9			55	18	9			38	16	12			24	6	2		
04	138	5	12		117	9	22			95	13	11			86	14	13			68	14	6		р	55	18	10			35	14	- []			24	7	1		
05	132	5	11		103	8	20			85					80	10	ι3			68	11	13			51	18	13			3 <i>5</i>	14	14			27	5),		
06	130	7	13		103	14	II			81	8	14			83	10	6			60	10	16			51	7	12			31	18	9			28	5	3		
07	128	8	16		105					81*					જ મ	11	8			50	10	12			49	13	14			27	14	9			27	3	Z		
08	124	σı	16		101	15	15			79-	8	14			82	જ	6			40	20	5			35	13	6			27	14	8			25	4	S		
09	124	14	17		98					75*					83	10	4			38	ız	6			35	GI	9			28	8	9			25	2	3		
10	126	9	15		98	15	15			75	12	12			86	7	9			38	10	6			29	18	6			29	10	9			26	7	3		
11	128	ol	17	,	97	ŞΙ	10			18	29	13			94	22	16			40	lo	6			31	4	7			27	Ħ	6			26	6	3		
12	131	18	14		105	20	16		- 11			14			88	٥٢	24	-		44	33	10			33	Ş١	6			28	25	6			28	14	5		
	136	T	_		115	20	24					27			96	13	27			46	42	SI			51	6	24			30	20	12			31	13	5		
	138				116	21	16			99	18	20			94	16	Zø			66	20	30			49	18	ટા			33	21	15			35	0	8		
	140				119	16	26		- 11	102		22				19				67		-			49	16	12			38	20	20			35	9	6		
	143	_			124	6	19			Sai		17			96	16	20			10	18	ζo			54		13			39	15	15			36	lì	9		
17	141	h	10		118	11	lı		- 11	96		13			91		SI			68	16	8			56	13	7			43	14 ·	19			36	14	9		

98

96

94

99 20 15

103 24 13

10

105 7 13

101 10 9

99

101 11

16 27

8 16

10 18

94 19 15

92 12 19

94 10 12

118 15 Fam = median value of effective antenna noise in db above ktb

119 12 13

119 16 15

37

8

125 5

120 12

119 12

D_{ti} = ratio of upper decile to median in db

18

20

21

22

19 140

40

11 12

8

8

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8

De = ratio of median to lower decile in db

V_{dm}= median deviation of average voltage in db below mean power Ldm = median deviation of average logarithm in db below mean power TABLE 4

δ

8 6

14 12

6

76 12 8

77 9

76 8

13

59

60

61

59

17

20

17

5 58

4

RN-13

38 15

39 10 15

38

29

27 5 5

1,3

39 22

13

10

43 10

43 9

41

39

20

21

19

15/01

39 10 16

MONTH-HOUR	VALUES	OF	RADIO	NOISE

Station São José, Brasil	Lat. 23.39S Long. 45.89W	Month December 19 63
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E									-		_						Fre	eque	ency	(1	Mc)]
(LST)			.05	1			. 1	13				. 24	6				545	1				2.5					5.0					0.0)				0.0		1
Hour	Fam	Du	, 	Vdm Ldm	Fam	Du	De	Vdm	Ldm	Fam	Du	D,	Vdm	└dm	Fam	Du	De	V _{dm}	Ldm	Fam	Du	D _Z	Vdm	L _{dim}	Fam	Du	D _Z	Vdm	∟dm	Fam	Du	De	Vdm		Fam			Vdm Ldm	4
00	134	7	8		ΙD	14	४			103	14	10			87	17	7			71	Ю	8			55	10	18			43		17					5		┨
01	133	9	9		10%	15	8			105	14	11			88	15	9			71	6	9			51	6	го			41	12	6				23	2		4
02	132	9	10		106	14	7			101	13	()			87	16	10			71	8	10			55	7	16			39	10	7		_	24	15	2		-
03	132	8	20		106	14	10_			101	12	12			84	15	6			71	7	10			53	8	15			39	8	9			24	16	2		4
04	132	8	26		llo	14	16			97	12	8			81	14	6			69	8	10			<i>5</i> 3	10	16			30	Щ	Ŷ			24	8	2	 	-
05	127	9	29		93	13	5.	L		81	13	8			75	8	5			65	8	14			50	17	13			37	8	4			24	21	2		┨
06	121	13	5		93	10	11			85	16	16			85	7	11			<u>55</u>	10	8			46	19	9	<u> </u>		35	Įį.	6		-	24	18	2	- 	4
07	116	15	7		92	12	8			79	18	6			83	8	10	L		47	ŧŧ.	9	ļ		42	14	6			32	9	5			24	Н	2		4
08	119	11	8		92	10	5			શ	8	8			85	8	8			39	13	14	L.		43	-	8			32	9	7			24	4	2	├├-	4
-	120	9	15		94	10	10			79	8	2			85	4	12			39	8	4			39	8	5			31	8	8			24	4	2		4
10	119	9	13		94	7	12			₹3	8.	8	<u> </u>	<u> </u>	₹5	5	8	<u> </u>		38	1	5			38	7	7			27	10	6			24	2	2		4
11	122	9	16		94	14	5		<u> </u>	83		9		<u> </u>	87	6	14			39	+	6			37	4_	6	_		29	10	4	<u> </u>	_	24	6	4	\vdash	4
12	128	13	12		100	25	10			91	31	12			87	23	14			41	25	6			37	20	5			35		1.0			24	13	5	├┼-	┨.
13	131	24	17		105	30	19				26	22			91	28	12			53	21	16	<u> </u>		43	18	8	<u> </u>	ļ		22	11	<u> </u>		28	15	6	\vdash	4
14	133	10	16		112	2	1 23			106	23				87	24	6			59	-		<u> </u>		45	20	14	<u> </u>	_	41	B	12			29	17	5	┝╌┝╌	H
15	136	17	17		113	25	22			109	22	28	L	•	89	25	8	_	L	59	+	22		<u> </u>	51	16	16	 	<u> </u>	46	13	14			3,2	17	8		+
16	144	η	22		113	23	22			10 8		27	_		91	27	13	<u> </u>	_	и——	28	23	ļ	<u> </u>	53	_	17	<u> </u>	+	45	12	_	_		34	14	8		-
17	136	16	20		118	14	26			111	14	34			89	22	_			61	20		 	<u> </u>	59	+ -	19	+	_	39	1	8	—		32	18	4		4
18	135	12	18		118	12	26		<u> </u>	112	9	25	<u> </u>		91	13	13	<u> </u>		66	13	10	ļ	<u> </u>	60		16	+		47	12	6	ļ	<u> </u>	34	19	1	 	4
19	-		14		114	11	17			106	12	15		ļ	89	14	6	<u> </u>		73	9	1		ļ	63		16	_		47	14	6	┼—		28	27	4		\dashv
20	135	8	4		11	1 10	12		\perp	103	_	12	<u> </u>	ļ	91	13	8	<u> </u>	_	74	7	13	 	<u> </u>	63	┿	16	1		47	13	K	ļ	<u> </u>	28	28	6		\dashv
21	136	7	14		117	1 11	10			105	5 14	10			91	12	8		<u> </u>	72	9	11	ļ	↓_	61	8	20	1"	 	-	12	4			28	21	6		\dashv
22	135	8	51		m	14	7	$oxed{oxed}$		105	13	10	_	$oldsymbol{ol}}}}}}}}}}}}}}}}}$	91	12	8	_	_	73	6	12	_	_	61	10	20		-	45	10	4	-	<u> </u>	26	28		+	+
23	134	8	6		ηλ	10	12			105	14	16			189	17	16		<u> </u>	73	6	12	<u>. </u>	<u></u>	61	111	24	<u>L</u>		44	10_	3	<u>L</u>	<u> </u>	24	26	یے		زل

 $\mathbf{F}_{\mathbf{drm}}$ = median value of effective antenna noise in db above ktb

Du = ratio of upper decile to median in db

Dg = ratio of median to lower decile in db

V_{dm}= median deviation of average voltage in db below mean power

L_{dm} = median deviation of average logarithm in db below mean power

TABLE 5

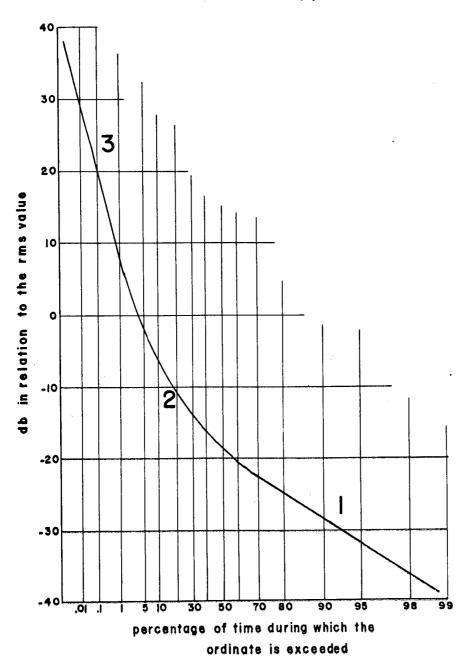


Fig. 1 - Amplitude Probability Distribution Curve
for Atmospheric Noise

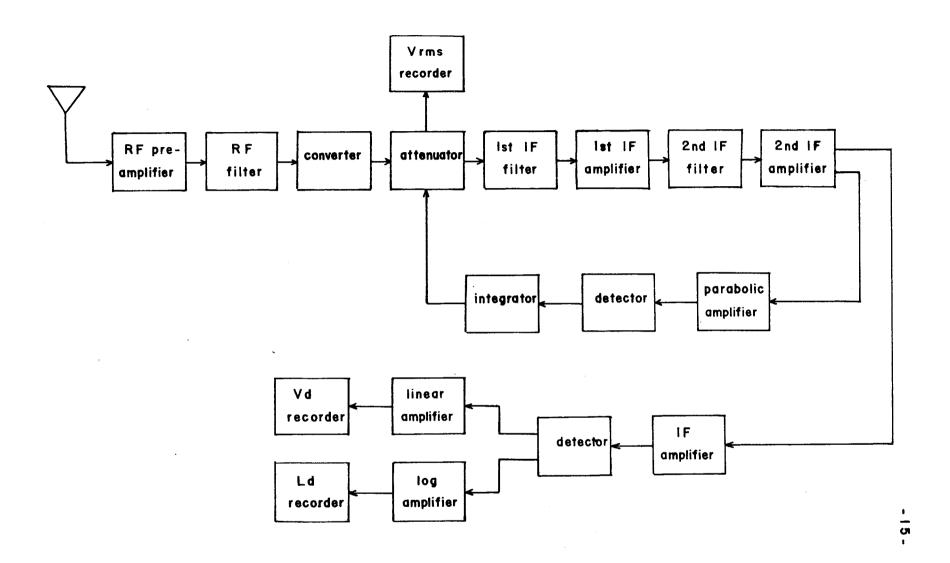


Fig. 2- ARN-2 block diagram for one channel

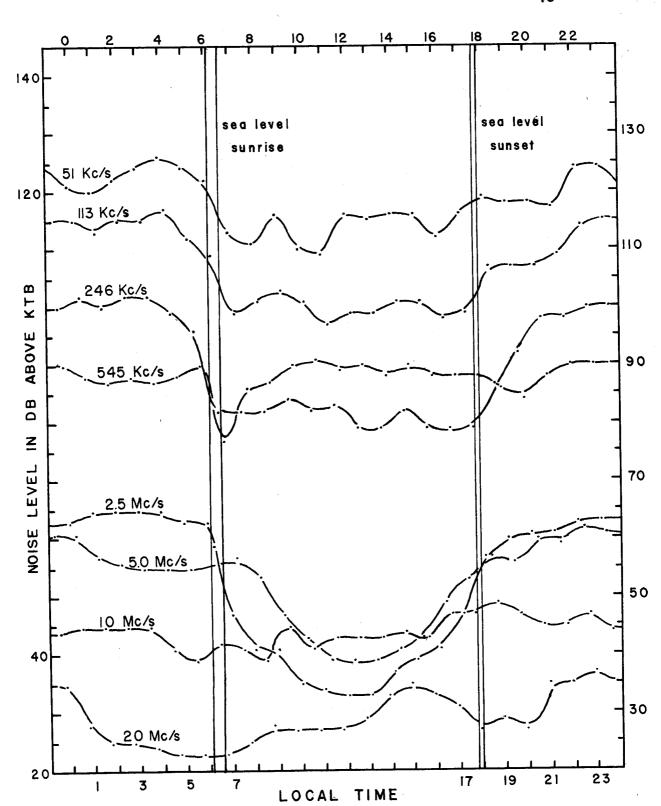


Fig. 3- Monthly Median Values for August 1963

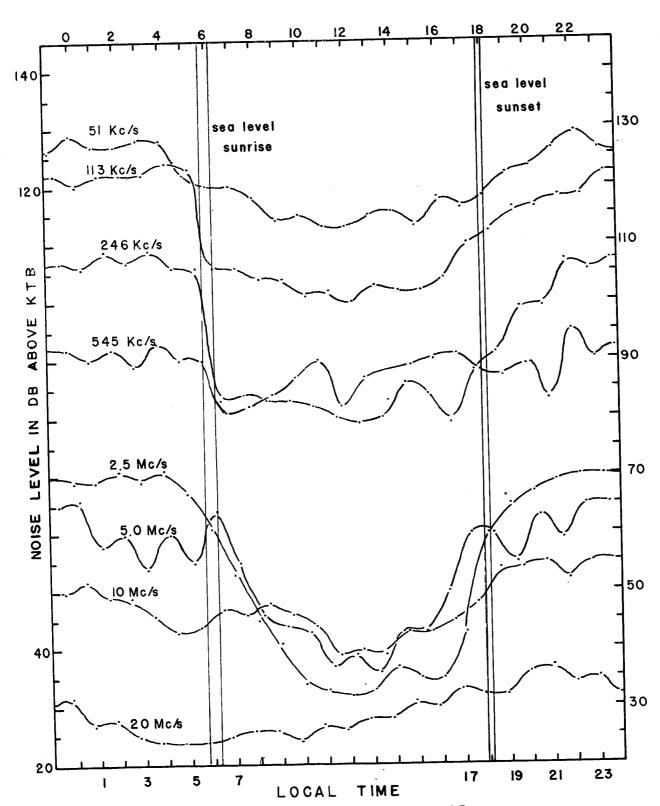


Fig. 4- Monthly Median Values for September 1963

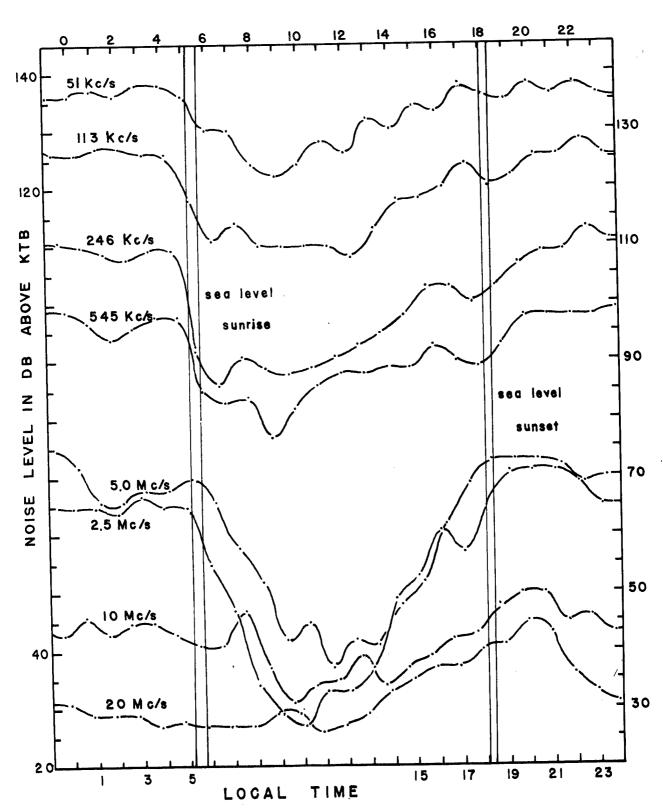


Fig. 5 - Monthly Median Values for October 1963

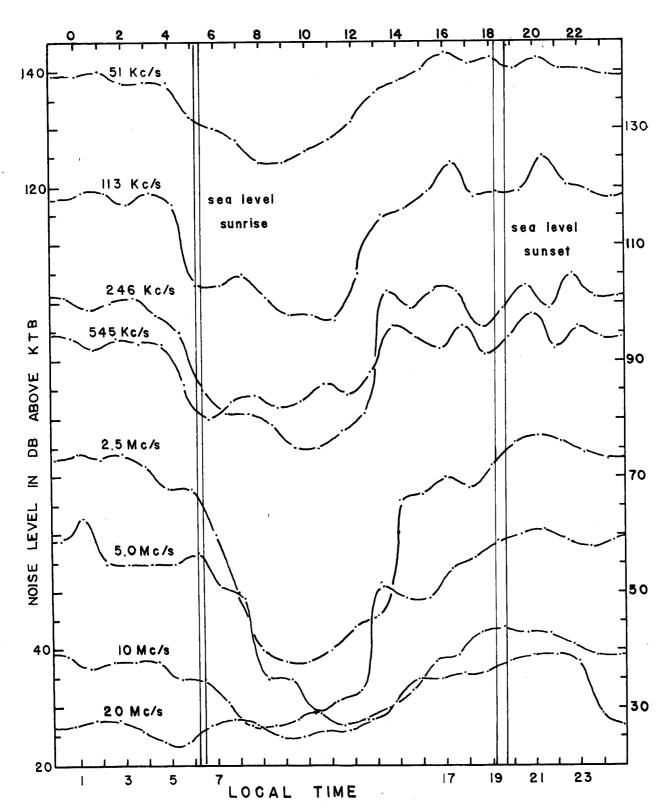


Fig. 6 - Monthly Median Values for November 1963

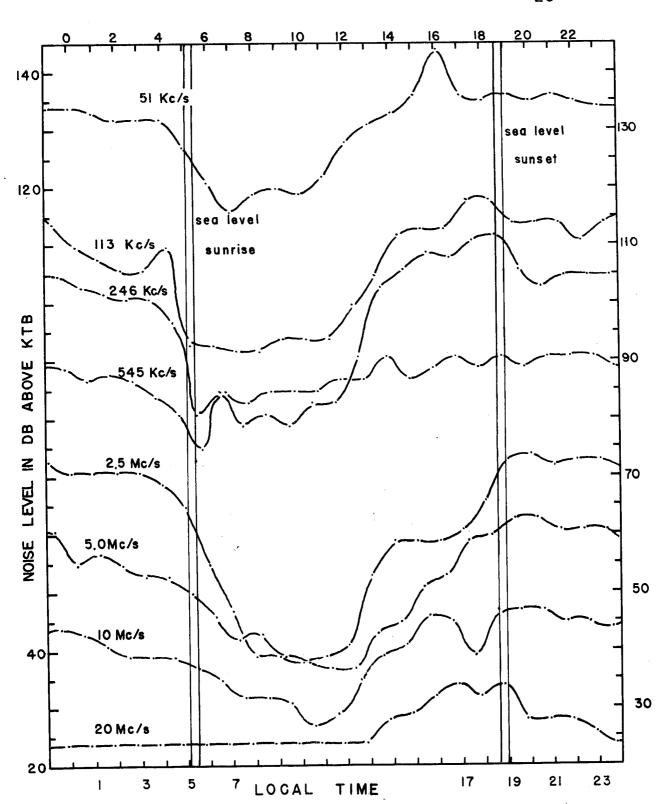


Fig. 7 - Monthly Median Values for December 1963

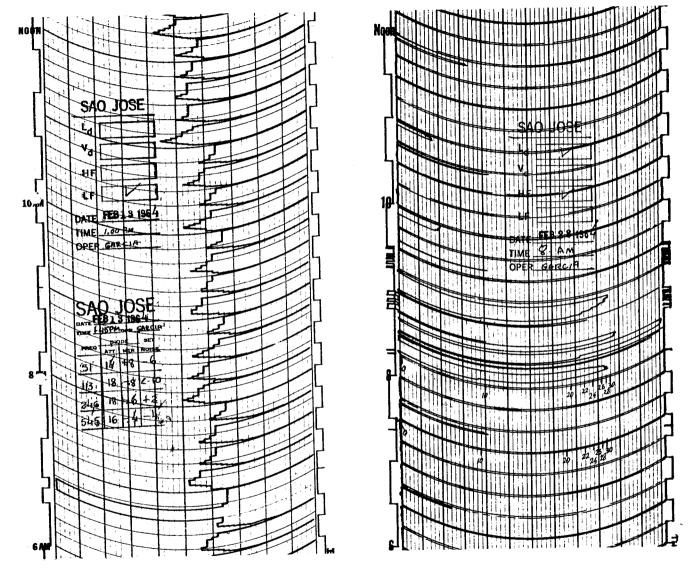


Fig. 8 - Recorder Charts

a) Log deviation

b) power

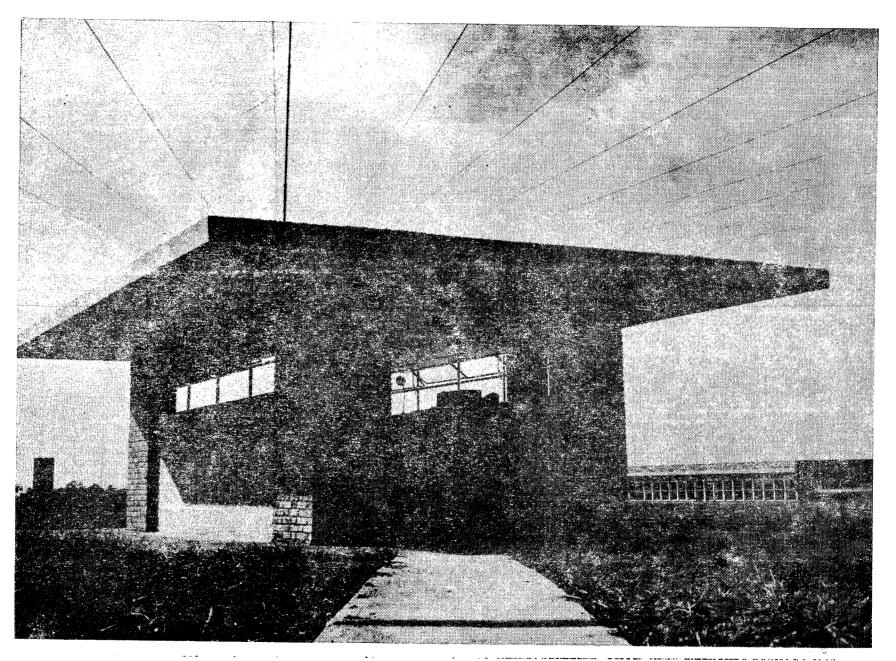


FIGURA 9 - BUILDING OF ARN-2 STATION Nº 10 IN SÃO JOSÉ DOS CAMPOS

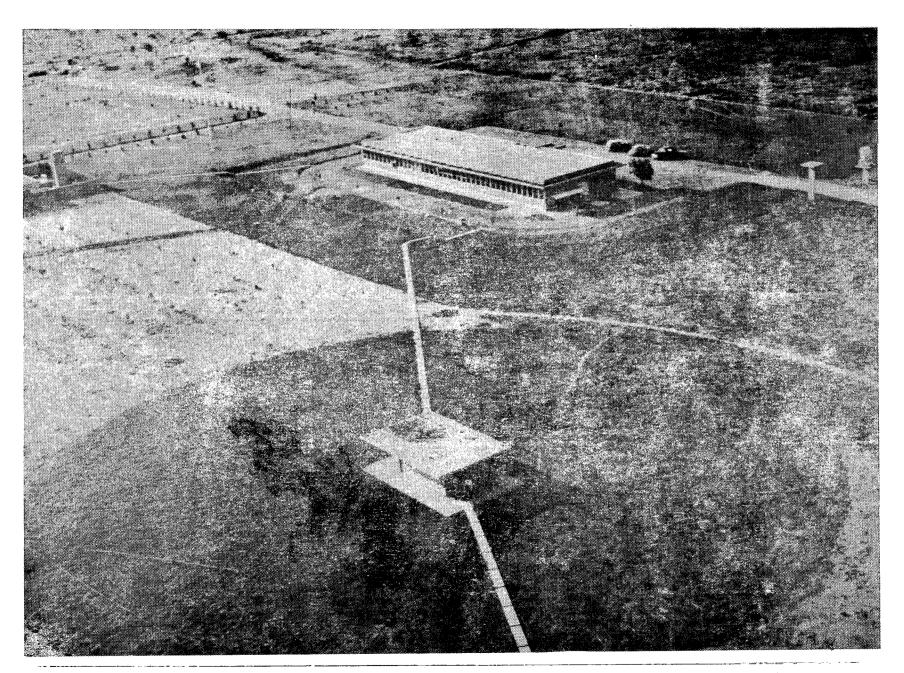


FIGURA 10 - ARN BUILDING IN THE FOREGROUND AND MAIN LABORATORY IN THE BACKGROUND

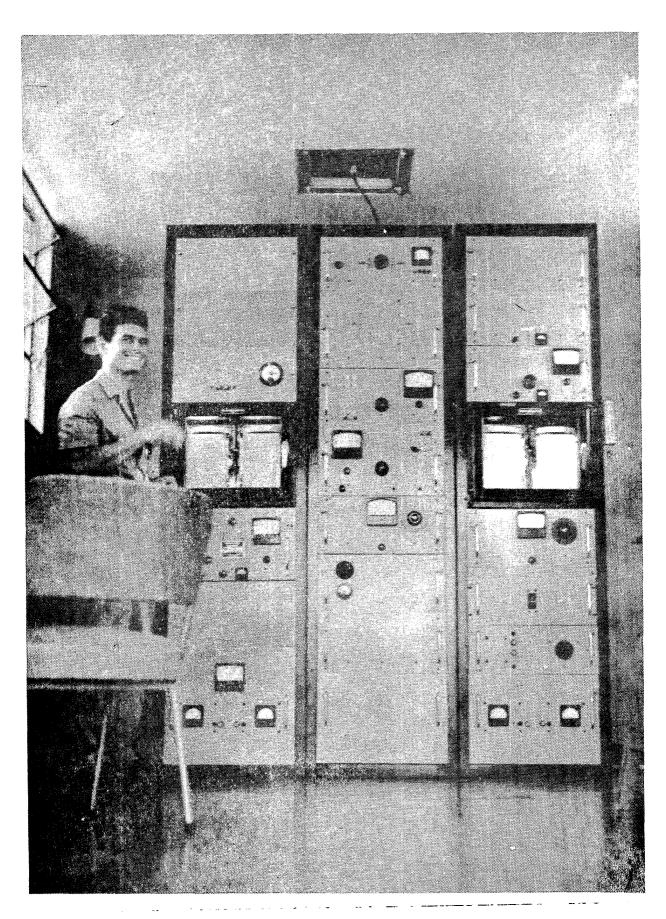


FIGURA 11 - ATMOSPHERIC RADIO NOISE RECEIVING EQUIPMENT